1 Introduction

Northrop Consulting Engineers were engaged by EJE Architecture to undertake a Concept Stormwater Management Assessment for the proposed development of Kendel Park Environmental Village in Burton Road, Mount Hutton. It is intended that the Stormwater Management Assessment form part of the documentation to support a Development Application for the proposed works.

1.1 Aim

The objective of the Concept Stormwater Management Assessment was to determine existing site constraints in regards to stormwater and drainage, as well as the effect the proposed development will have on water quality and quantity, both within and downstream of the site. This assessment further aims to identify appropriate processes for the control of both sediment and pollutants generated onsite, and to present an appropriate solution for onsite stormwater detention.

The Concept Stormwater Management Plan presented in this report has been designed with Lake Macquarie City Council's (LMCC) DCP No.1 in mind, and has endeavoured to comply with all the requirements of this document.

This report is intended to discuss Stormwater Management issues at a level appropriate for a Development Application. It does not attempt to provide detailed design solutions to all issues; rather it investigates the feasibility of achieving solutions based on information that we have gathered to date from a number of sources.

1.2 Site Characteristics

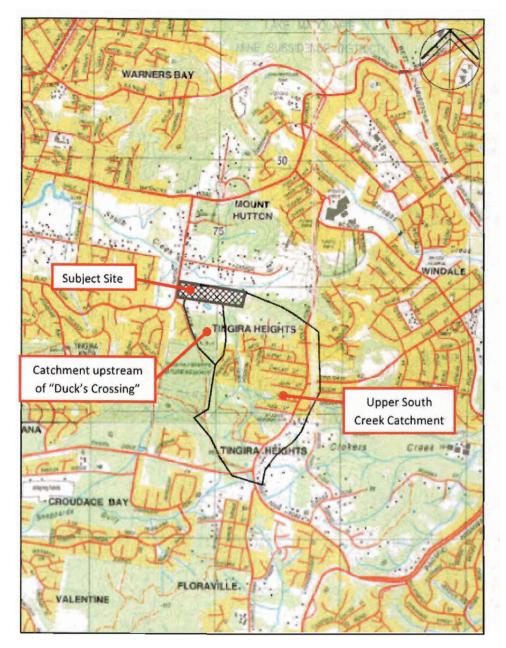
The 4.95ha site of the proposed development, consisting of Lots 11 and 12 in DP 830292, is hereafter referred to within this report as "the subject site".

The subject site is bounded by Burton Road to the west, and private residential land to the north, east, and south. The site is situated in the upper area of the South Creek catchment, and a portion of South Creek traverses the rear of the site. The rear area of the site (approx 0.8ha) grades towards South Creek, whilst the majority of the site slopes generally to the north-west away from South Creek. The front area of the site grades more generally to the north. Existing site grades are gentle, typically averaging 3%.

The subject site currently accommodates two residences, and associated buildings including stables and garages. The majority of the site is cleared rural land, with some established disperse vegetation.

An existing stock dam is situated near the southern boundary of the subject site. Existing dams situated on the property to the south of the site, 'Duck's Crossing', appear to currently drain through the subject site near the site's dam, (without an easement), toward a vegetated drainage path located on the property to the north of the subject site. This drainage path appears to discharge into an existing table drain situated along Burton Road.

Figure 1 overleaf depicts the site location and upstream catchments.



Note: Maps extracted from the Wallsend and Swansea 1:25 000 Topographic Maps.

Figure 1 - Site locality and upstream catchments

2 Stormwater Management

2.1 Overview

The proposed development consists of 51 of residential units, a community centre, and associated roadways, which will increase the impervious area of the subject site. This increase in impervious area will increase both peak flows and the concentration of pollutants within stormwater runoff from the site. Stormwater management devices will be adopted within the proposed development to mitigate peak flows from the site and treat stormwater pollutants to acceptable levels.

In broad terms, it is proposed that surface runoff from the subject site be directed towards a formal road drainage system comprising a series of pits and pipes, before being discharged into an aboveground stormwater detention system. The detention system will be designed to detain flows directed to it, such that peak developed flow from the entire subject site is limited to the peak predeveloped site flow, for storm events up to and including the 1 in 100yr ARI event. Controlled flow from the detention system will be directed to Burton Road¹. It is proposed the detention system be constructed as a bio-detention system to serve a dual purpose, and filter stormwater pollutants prior to stormwater exiting the site.

Additional stormwater treatment and peak flow detention will be provided on site via rainwater tanks which are proposed to be connected to each unit to harvest roofwater for reuse.

It is proposed an overland stormwater drainage path be maintained through the subject site to safely convey flow derived offsite to a downstream outlet point.

2.2 Upstream Flows

As indicated in Figure 1, an upstream catchment estimated to be 13ha drains towards the subject site through the "Ducks Crossing" property located to the south. The "Duck's Crossing" property currently has a dam situated adjacent to the subject site's southern boundary, which appears to mitigate upstream flows. This dam appears to currently overflow into the subject site, through the subject site's dam, and into a drainage path located on the property north of the subject site. The proposed development layout has been designed to maintain an overland flow path through the subject site to safely convey this upstream flow to the existing drainage path downstream of the subject site.

A section of South Creek passes through the rear of the subject site, as indicated in Figure 1. Detailed survey of the subject site indicates the proposed development will drain away from, rather than toward South Creek, and will therefore not alter the existing flow or flood regime through the rear of the site. Flow and flooding characteristics for this section of South Creek are discussed in Section 2.3 of this report.

¹ The geometry of the existing table drain in Burton Road downstream of the site has adequate capacity to convey the peak 100 year ARI flow from the proposed detention basin. It is required to convey the 10 year flow in accordance with Council's Engineering Guidelines Part 1. Refer to Appendix C for further detail.

Flooding 2.3

As previously noted, the subject site is situated within the upper reach of the South Creek catchment, and a portion of South Creek passes through the rear of the site. The Lake Macquarie City Council South Creek Flood Study (Draft April 2010, prepared by Cardno) suggests that areas of the subject site could be inundated in the 1% AEP and PMF rainfall events.

To assess the potential for flooding within the subject site, and the impact of the proposed development on local flood regimes upstream and downstream of the subject site, flood modelling based on detail survey has been undertaken in collaboration with Cardno.

Based on the flood modelling completed by Cardno we have reproduced on CO9DA (refer Appendix B) the 1% AEP and PMF flood extents for the developed site. In accordance with the 'Flood Management Manual (Jan 2001)' we provide the following advice regarding the design of the development with relation to flood levels:

- > Developable areas on site are proposed to be raised above the 1% AEP flood extents.
- > Finished Floor Levels for dwellings across the site are proposed to be set a minimum of 500mm above the 1% AEP flood levels adjacent to developable land.
- > The PMF extent covers the majority of the site. The exception to this is an area on the eastern development pad adjacent to Burton Road; Units 23-30; Units 49-51; and Units 37-41. In these areas the FFL have been set at or just above the PMF level. Furthermore it is noted that the PMF depth across the development area of the site is minor ranging from 0-400mm. As such, the results of the PMF modelling show that there are sufficient areas on site which can act as safe refuge in the event of a PMF.

Further detailed discussion on the Flood Modelling results are presented in the Flooding Report completed by Cardno.

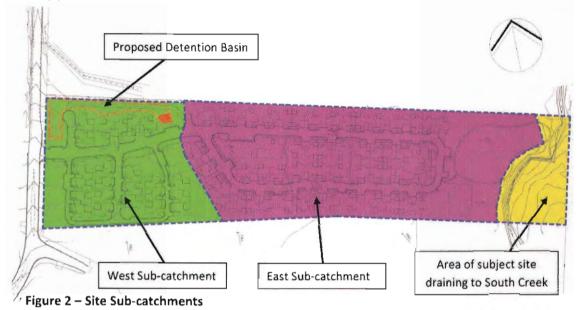
On-site Detention

2.4.1 Methodology

Lake Macquarie City Council's DCP No. 1 & 2 requires the Concept Stormwater Management Plan to show how peak developed flow from the site can be appropriately limited to that expected from the pre-developed site, for all events up to and including the 1% AEP event. It is proposed that this will be best achieved on site via an aboveground detention system, in combination with underground rainwater tanks.

It is proposed the detention basin be located in the north-western corner of the developed site, and discharge flows to Burton Road. The detention basin will be wide and shallow (0.5m depth) to enable integration with existing site levels and vegetation, and the proposed fire-trail.

Based on existing surface grades, which will generally be maintained post development, the subject site was divided into 2 sub-catchments for the purpose of detention modelling, as depicted in Figure 2 below. Runoff from each sub-catchment will be directed into the proposed detention basin via a pit and pipe network.



The runoff routing software XP_RAFTS was used to model peak flow from the sub-catchments. Model parameters include:

- Initial Loss and Continuing Loss parameters for pervious areas have been assumed to be 10mm and 2.5 mm/hr respectively.
- Initial Loss and Continuing Loss parameters for impervious areas have been assumed to be
 1.5 mm and 0 mm/hr respectively.
- Pre-developed sub-catchments were assumed to be 100% pervious.

Table 1 outlines sub-catchment areas and the impervious fractions modelled for the developed state.

Table 1 - Sub-Catchment Parameters used in the XP_RAFTS Modelling

| Sub-catchment | Total Area (ha) | % Impervious (developed case) (roof areas and pavements) |
|---------------|-----------------|---|
| East | 2.9 | 32% |
| West | 1.6 | 40% |

The "Duck's Crossing" catchment was not included in the XP_RAFTS model, as flow from this catchment will be directed past the detention basin toward the existing drainage path to the north of the site, as noted in previous sections of this report.

2.4.2 Detention Facility

A detention basin for the development was designed using the XP_RAFTS model, to detain flows such that peak flow from the developed site does not exceed peak flow pre-development across rainfall events up to and including the 1% AEP event.

The detention system was modelled as an above ground basin with a top water level of 10.80m AHD, an invert level of 10.30m AHD and the stage / storage relationship shown in Table 2. The detention basin was designed with 2 x 450mm diameter orifice low flow outlets having an inlet invert at 9.55m AHD and downstream outlet invert at 9.45m AHD, and a high level overflow weir (5m long) having an invert of 10.6m AHD.

Table 2 – Basin Elevation versus Storage Relationship

| Stage (m AHD) | Storage (m³/s) |
|---------------|----------------|
| 10.3 | 0 |
| 10.55 | 177 |
| 10.8 | 405 |

2.4.3 Hydraulic Modelling Results

To determine peak flow from the subject site, a range of storm durations were run in XP_RAFTS for a range of AEP's. A summary of the peak results are shown in Table 3 overleaf, while results for all durations and AEP's are shown in Appendix A.

Table 3 - Peak Flow Results from the XP RAFTS Modelling

| AEP | 20% AEP m³/s | 10% AEP m ³ /s | 5% AEP m³/s | 2% AEP m³/s | 1% AEP m³/s |
|-----------------------------|-----------------|----------------------------------|----------------|----------------|----------------|
| Pre-developed | 1.0 | 1.1 | 1.4 | 1.5 | 1.7 |
| Developed (with detention.) | 0.8 | 0.8 | 1.1 | 1.4 | 1.6 |

As shown in Table 3, peak post-developed flow is limited by the proposed detention basin to below pre-developed flow for all storm events modelled. The modelling found the peak storage required to detain the 1% AEP storm event to be 395m³, which occurred at a stage of 10.79m AHD.

This is a conservative estimate for the proposed detention basin size and performance, as it assumes the proposed rainwater tanks for each dwelling do not contribute to stormwater detention during. peak rainfall events. In reality, it is likely that there will be some storage capacity available within the rainwater reuse / storage tanks, and the tanks will be designed to perform this dual purpose.

2.4.4 Basin Safety

The proposed basin will be a dry basin, with no permanent water. Maximum temporary water levels within the basin will be 0.5m deep (proposed basin top water level 10.8m AHD, minimum proposed base level 10.3m AHD).

The proposed southern side of the basin consists largely of existing gently graded site levels, with grades max 1V:8H in line with the rear of the proposed residences. Appropriate vehicular access for maintenance can be readily achieved from a proposed cul-de-sac turning head to be constructed as part of the proposed Stage 2 works. The proposed mound forming the northern side of the basin will be situated adjacent to the northern boundary of the site, and planted and fenced in accordance with the proposed landscaping plan.

Planting / landscaping is proposed around the proposed basin inlets, where basin side batter slopes are maximum 1V:4H. This treatment is in accordance with Council's 'Batter Slope Treatments and Fencing Guidelines for Constructed Wetlands and Detention Basins' (2009) for basins with maximum 1V:4H side slopes and water depths less than 1.2m.

Review of Table 1 in Council's 'Batter Slope Treatments and Fencing Guidelines for Constructed Wetlands and Detention Basins' (2009) with regard to risk factors yields the following:

| 1. | Batter slopes above permanent water level | Risk Factor = 1 – 2 |
|----|---|---------------------|
| 2. | Vertical drop at water edge – below permanent water level | Risk Factor = 0 |
| 3. | Max water depth between water edge and 4m from the | Risk Factor = 4 |
| | water edge – below permanent water level | |
| 4. | Site context | Risk Factor = 4 |

Total Risk Factor Score <10

The required batter treatment and fencing requirement in accordance with Table 1 for the basin is therefore mown grass and/or planting for aesthetic and shade purposes.

2.5 Water Quality

2.5.1 Treatment

The development of the subject site and its change of use will likely increase pollutant loads within stormwater runoff from the site. In order to mitigate the increase in pollutants and protect downstream receiving waters, the proposed stormwater management concept includes a number of treatment measures. Stormwater Quality Improvement Devices (SQIDS) have been specifically chosen to form a treatment train through the subject site, such that all forms of pollutants will ultimately be mitigated.

The design of SQUIDS for the subject site has been completed in accordance with Lake Macquarie City Council's 'Stormwater Treatment Framework & Stormwater Quality Improvement Device Guidelines' (SQID Guidelines). In accordance with Table 2.1 of this document, residential developments greater than 2ha are required to treat stormwater runoff to the following target pollutant removal levels:

Gross pollutants: 50-100% reduction

Course Sediments: 50-100% reduction

Medium Sediments: 30-80% reduction

Fine Sediments: 30-50% reduction

Nutrients: 30-50% reduction

Heavy Metals /Oils and Greases: 30-50% reduction

The SQUIDS treatment train proposed for the development was modelled using the continuous simulation software MUSIC, to assess the likely pollutant reduction. The MUSIC model used observed rainfall data taken from Williamtown Airport over a period of 7 years from 2000-2007. Figure 3 overleaf presents a screen shot of the MUSIC model compiled for the subject site.

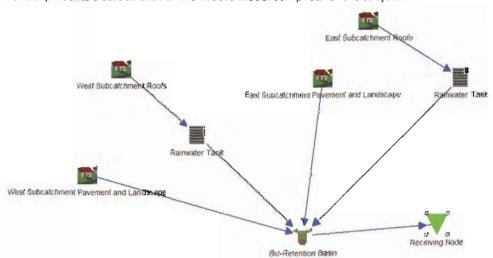


Figure 3 - MUSIC model Schematic

As illustrated in Figure 3, the MUSIC model was based around the two site sub-catchments described in Section 2.4. A summary of the SQIDS proposed for the development, how they were modelled in MUSIC, and how they will are proposed to be incorporated within the subject site is as follows:

- First Flush Diverters Runoff from the roofs of all proposed Units (likely containing small amounts of phosphorus and dust particles) will be treated by first flush devices attached to all downpipes. By capturing the first portion of runoff from roofs, the first flush devices will effectively remove dead insects, bird and animal droppings, and concentrated tannic acids from the stormwater system. Runoff captured by first flush devices will, in accordance with common practice, be emptied from the devices into landscaped areas at a rate of approximately 1 L/hr. It is proposed that leaves and gross pollutants be filtered from runoff via mesh filters fitted to downpipes. It should be noted that first flush devices were not modelled in MUSIC, making the modelled pollutant removal results somewhat conservative.
- Roof Water Tanks Runoff from roof areas of all proposed Units will be collected in downpipes and directed to minimum 3kL underground rainwater tanks, proposed to be

located below the rear courtyard of each unit. Roofwater tanks will effectively act as sediment traps, collecting fine sediment and nutrients attached to sediment particles. Reused water from the tanks will limit the volume of runoff leaving the site, as well as removing pollutants contained in the water. MUSIC modelling assumed that each unit would reuse approximately 80L/day for toilet flushing, clothes washing and external irrigation. Based on an average daily water use of 400L/day for each unit this equates to roughly 20% of total usage. This volume of reuse is considered conservative when compared to relevant literature which suggests toilet flushing and irrigation make up ~30% of total water use.

Bio-retention Basin – The proposed detention basin will function as a bio-retention system, as it is intended to have highly permeable upper soil layers planted with water tolerant plants in keeping with local vegetation. The vegetation and permeable soil mediums will treat stormwater to remove fine sediments and nutrients. A rock-lined and vegetated stilling basin will be incorporated into the basin design to slow and disperse flows within the basin, and provide initial water quality treatment. The fire trail area within the basin has been assumed to be impermeable for the purposes of MUSIC modelling.

2.5.2 MUSIC Modelling Results

While MUSIC does not model all pollutants noted in LMCC's SQUID guidelines, it is noted that 'Total Suspended Solids' in MUSIC include fine and medium sized particles, and the removal process for Nitrogen and Heavy Metal are very similar, in regards to the form of treatment being provided. Table 4 below outlines the results of the MUSIC modelling.

Table 4 - MUSIC Modelling Results

| | Source | Residual | % Reduction | % Reduction Required |
|--------------------------------|----------|----------|-------------|-------------------------|
| Total Suspended Solids (kg/yr) | 3.49E+03 | 1.04E+03 | 70.2 | 50-100% |
| Total Phosphorous (kg/yr) | 7.62 | 3.68 | 51.8 | 30-50% |
| Total Nitrogen(kg/yr) | 57 | 38.1 | 33.3 | 30-50% |
| Gross Pollutants(kg/yr) | 571 | 0 | 100 | 50-100% |

From the output of the MUSIC modelling it can be seen that the treatment train proposed for the subject site will meet Lake Macquarie City Council's water quality guidelines.

2.6 Site Discharge Index (SDI)

SDI is defined by Lake Macquarie City Council (LMCC) as 'the ratio of the impermeable area that drains directly to a drainage system to the total site area' (LMCC Handbook of Drainage Design Criteria, 2004). LMCC require at least 90% of stormwater runoff from impervious areas of a site to be

managed through suitably designed stormwater controls, to achieve a desired SDI of no more than 0.1.

Proposed stormwater controls to treat runoff from the subject site include:

- Rainwater reuse tanks on all units, to treat and manage roof water runoff.
- Bio-retention basin to treat and manage runoff from paved surfaces.

All site flows from impervious areas can be directed toward the bio-retention basin, effectively rendering the SDI for the proposed development to be zero. Therefore, LMCC requirements for the proposed development can be readily met in regards to SDI.

3 Staging

The proposed development consists of 51 units and a community centre, with associated roadways, driveways and footpaths. It is understood that the development is likely to be undertaken in 5 stages, with construction commencing nearest to Burton Road and progressing toward the rear of the site.

The stormwater management concept for the development discussed in this report could readily accommodate staged construction. The proposed basin should be constructed during the first stage of the development, and stormwater infrastructure extended as the development progresses upstream.

4 Conclusion

The proposed development will require the incorporation of a number of stormwater initiatives and devices to mitigate and manage stormwater runoff from the site and from upstream sources. The stormwater concept outlined in this report will suitably mitigate and manage stormwater impacts within and downstream of the subject site. Upstream flows can be effectively managed and safely conveyed through the site without impacting on the proposed development. Stormwater management for the proposed development can be appropriately designed to suit construction staging.

It is reiterated that this Stormwater Management Assessment has been undertaken to discuss stormwater management issues at a conceptual level appropriate for a Development Application. It does not attempt to provide detailed design solutions to all issues; rather, it identifies that stormwater quantity and quality can be appropriately managed within the proposed development.

Appendix A - Detention Modelling Results

XP_RAFTS Modelling Results:

Table B1 - Flow rates from the Pre-developed subject site

| Duration | 20% AEP m³/s | 10% AEP m³/s | 5% AEP m³/s | 2% AEP m³/s | 1% AEP m³/s |
|----------|-----------------|-----------------|----------------|----------------|----------------|
| 10 | 0.2222 | 0.3138 | 0.4194 | 0.5985 | 0.7709 |
| 25 | 0.5407 | 0.69 | 0.8739 | 1.162 | 1.384 |
| 30 | 0.6512 | 0.7992 | 0.982 | 1.189 | 1.378 |
| 45 | 0.7244 | 0.8542 | 1.011 | 1.238 | 1.394 |
| 60 | 0.8452 | 0.9916 | 1.218 | 1.45 | 1.679 |
| 90 | 0.8982 | 1.061 | 1.325 | 1.548 | 1.741 |
| 120 | 0.9524 | 1.133 | 1.356 | 1.527 | 1.747 |
| 180 | 0.682 | 0.8346 | 0.9967 | 1.144 | 1.293 |
| 360 | 0.5711 | 0.6547 | 0.7681 | 0.8438 | 0.9491 |
| 540 | 0.4934 | 0.5678 | 0.6685 | 0.7403 | 0.8272 |

Table B2 - Flow rates from the Developed subject site, with the basin

| Duration | 20% AEP m³/s | 10% AEP m ³ /s | 5% AEP rm³/s | 2% AEP m³/s | 1% AEP rn³/s |
|----------|-----------------|----------------------------------|-----------------|----------------|-----------------|
| 10 | 0.493 | 0.5722 | 0.6815 | 0.7189 | 0.7607 |
| 25 | 0.6839 | 0.7231 | 0.7731 | 1.003 | 1.199 |
| 30 | 0.6634 | 0.7077 | 0.7742 | 0.9854 | 1.186 |
| 45 | 0.6304 | 0.711 | 0.8234 | 1.026 | 1.225 |
| 60 | 0.7157 | 0.7623 | 0.9834 | 1.232 | 1.416 |
| 90 | 0.7313 | 0.7794 | 0.9721 | 1.277 | 1.57 |
| 120 | 0.7548 | 0.842 | 1.128 | 1.373 | 1.56 |
| 180 | 0.6824 | 0.7168 | 0.7793 | 0.9552 | 1.1.23 |
| 360 | 0.5332 | 0.6047 | 0.6858 | 0.7173 | 0.7694 |
| 540 | 0.4663 | 0.5286 | 0.6161 | 0.6785 | 0.7119 |

Appendix B – Concept Drawings

KENDEL PARK ENVIRONMENTAL VILLAGE Burton Road, Mount Hutton. N.S.W.





DRAWING INDEX

DRAWING No. DRAWING TITLE

| C00 DA | COVER SHEET & DRAWING INDEX |
|--------|--|
| C01 DA | SEDIMENT & EROSION CONTROL PLAN |
| C02 DA | CONCEPT STORMWATER & LEVELS SITE PLAN |
| C03 DA | CONCEPT STORMWATER & LEVELS PART PLAN SHEET 1 OF 3 |
| C04 DA | CONCEPT STORMWATER & LEVELS PART PLAN SHEET 2 OF 3 |
| C05 DA | CONCEPT STORMWATER & LEVELS PART PLAN SHEET 3 OF 3 |
| C06 DA | CIVIL DETAILS SHEET 1 |
| C07 DA | CIVIL DETAILS SHEET 2 |
| C08 DA | CIVIL DETAILS SHEET 3 |
| C09 DA | FLOODING EXTENTS PLAN |
| | |

APPROVAL

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Ken Delforce

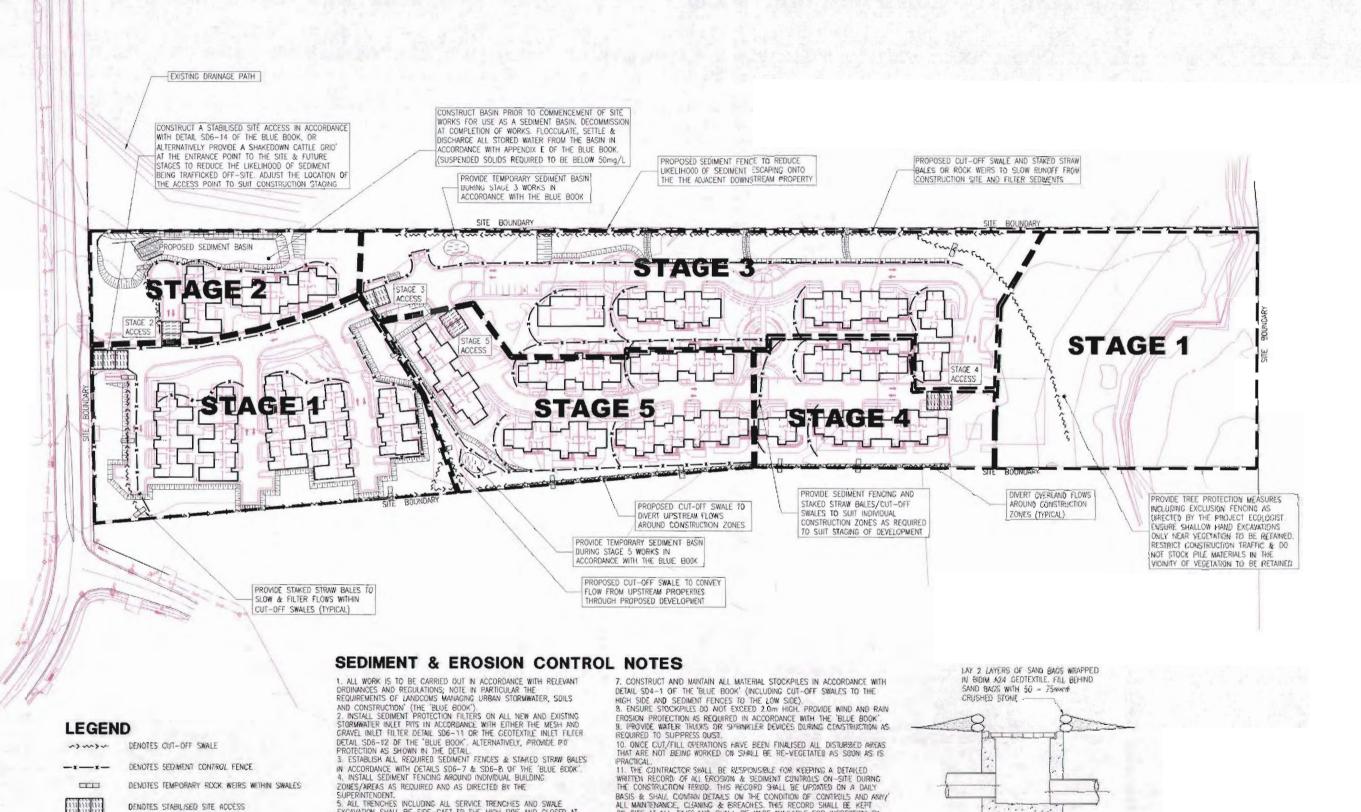
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Newcastle West
PH (07) 4079 2953

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KENDEL PARK ENVIRONMENTAL VILLAGE Burton Road, Mount Hutton. COVER SHEET &
DRAWING INDEX

NL 100073
DRAWING NUMBER ISSUE
COO DA D



STAGE OF THE DEVELOPMENT AT CC STAGE.

NOTE: A DETAILED SEDIMENT & EROSION

DEMOTES DIRECTION OF FALL IN MATURAL SURFACE

FALL

SUPERINTENDENT.

5. ALL TRENCHES INCLUDING ALL SERVICE TRENCHES AND SWALE.

EXCANATION SHALL BE SIDE-CAST TO THE HIGH SIDE AND CLOSED AT

THE END OF EACH DAYS WORK.

6. ENSURE THAT ALL VIGETATION (TREE, SHRUB & GROUND COVER) WHICH IS TO BE RETAINED SHALL BE PROTECTED DURING THE DURANDON

THAT ARE NOT BEING WORKED ON SHALL BE RE-VEGETATED AS SOON AS IS PRACTICAL.

11. THE CONTRACTOR SHALL BE RESPONSIBLE FOR KEEPING A BETAILED WHITEN RECORD OF ALL SECOSON & BEDMENT CONTROLS ON -SITE DURNG THE CONSTRUCTION TERROR. THIS PRECORD SHALL BE UPPRATED ON A DAILY BASIS & SHALL COMERN DETAILS ON THE CONDITION OF CONTROLS AND ARMY ALL MAINTENANCE, CLEANING & BREACHES, THIS RECORD SHALL BE KEFT ON-SITE AT ALL TAKES AND SHALL BE WADE AVAILABLE FOR INSPECTION BY THE PRINCIPAL CENTRYING AUTHORITY AND THE SUPPRINTENDENT DURING NORMAL WORKING HOURS.

12. PROVIDE SEDIMENT BASINS AND MAINTAIN DURING CONSTRUCTION IN ACCORDING WITH THE BILLE PROOF FOR EACH STACE OF WORKS.

ACCOMPANICE WITH THE BLUE BOOK FOR EACH STAGE OF WORKS.

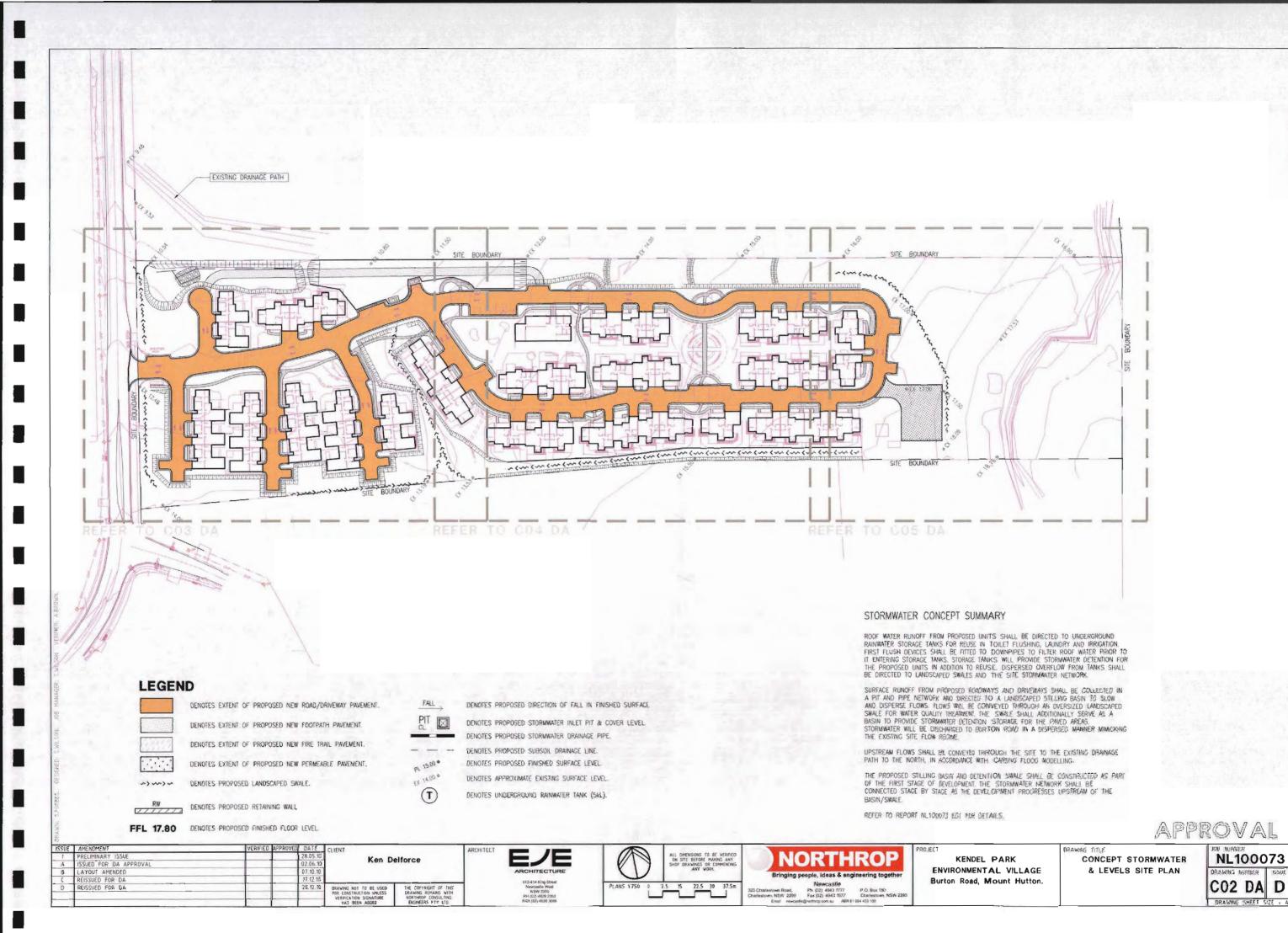
13. FLOCCULATE SETTLE AND DISCHARGE STORED WATER FROM THE TEMPORARY SEDAMENT BASIN, DISCHARGING WHEN SUPPENDED SOLIDS (SS) CONCENTRATION OROPS TO SOME THE THE WAS CONCENTRATION SHALL BE UNDERTAKEN PRIOR TO SOME TO SOME THE BASIN IN A DISPERSED AND CONTROLLED MANNER, CONDUCTED IN ACCORDANCE WITH APPENDIX E OF THE BLUE BOOK

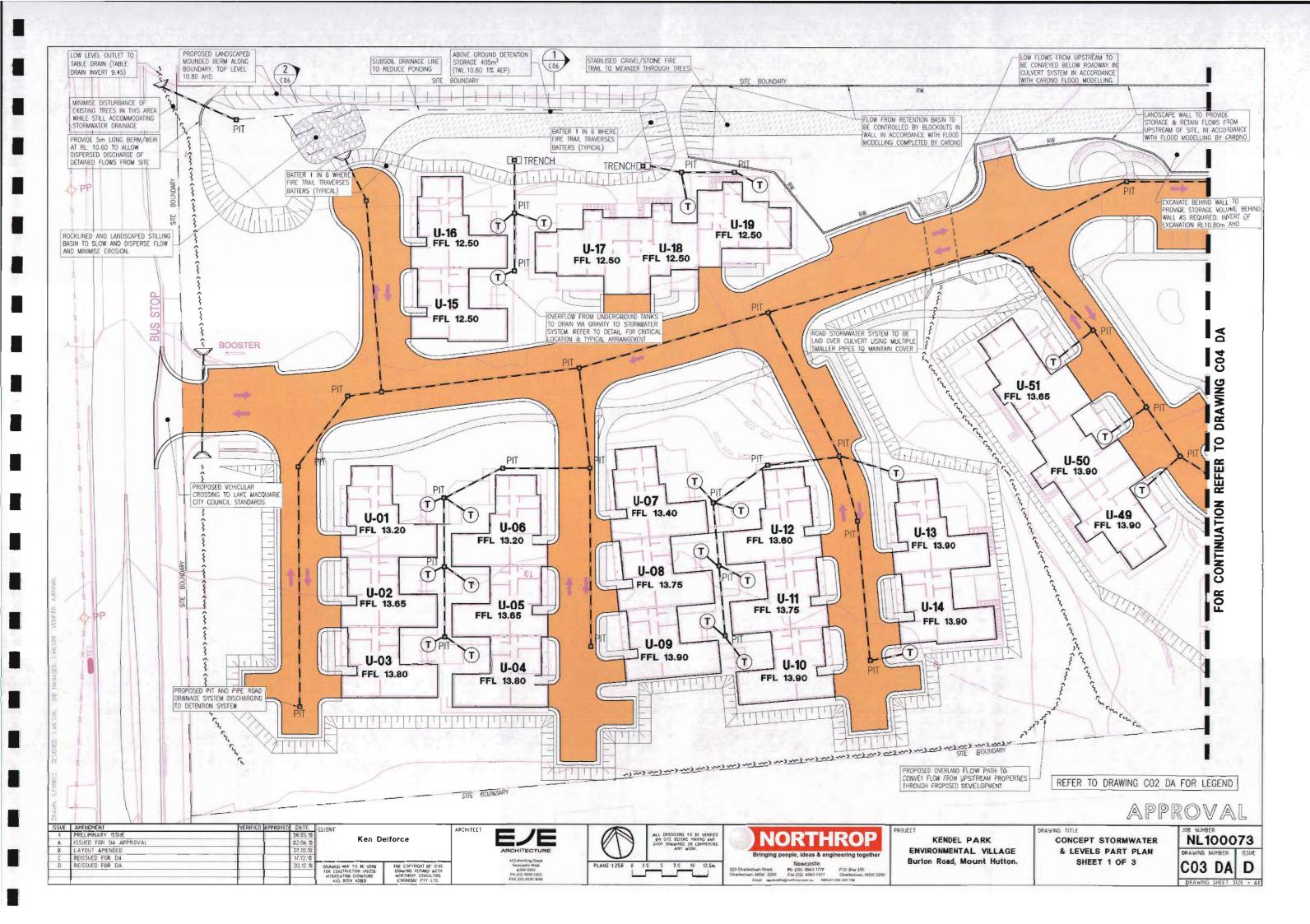
PIT PROTECTION DETAIL (ALTERNATIVE CETAIL SOS-11 OR SO6-12 OF THE BLUE BOOK AS APPROPRIATE)

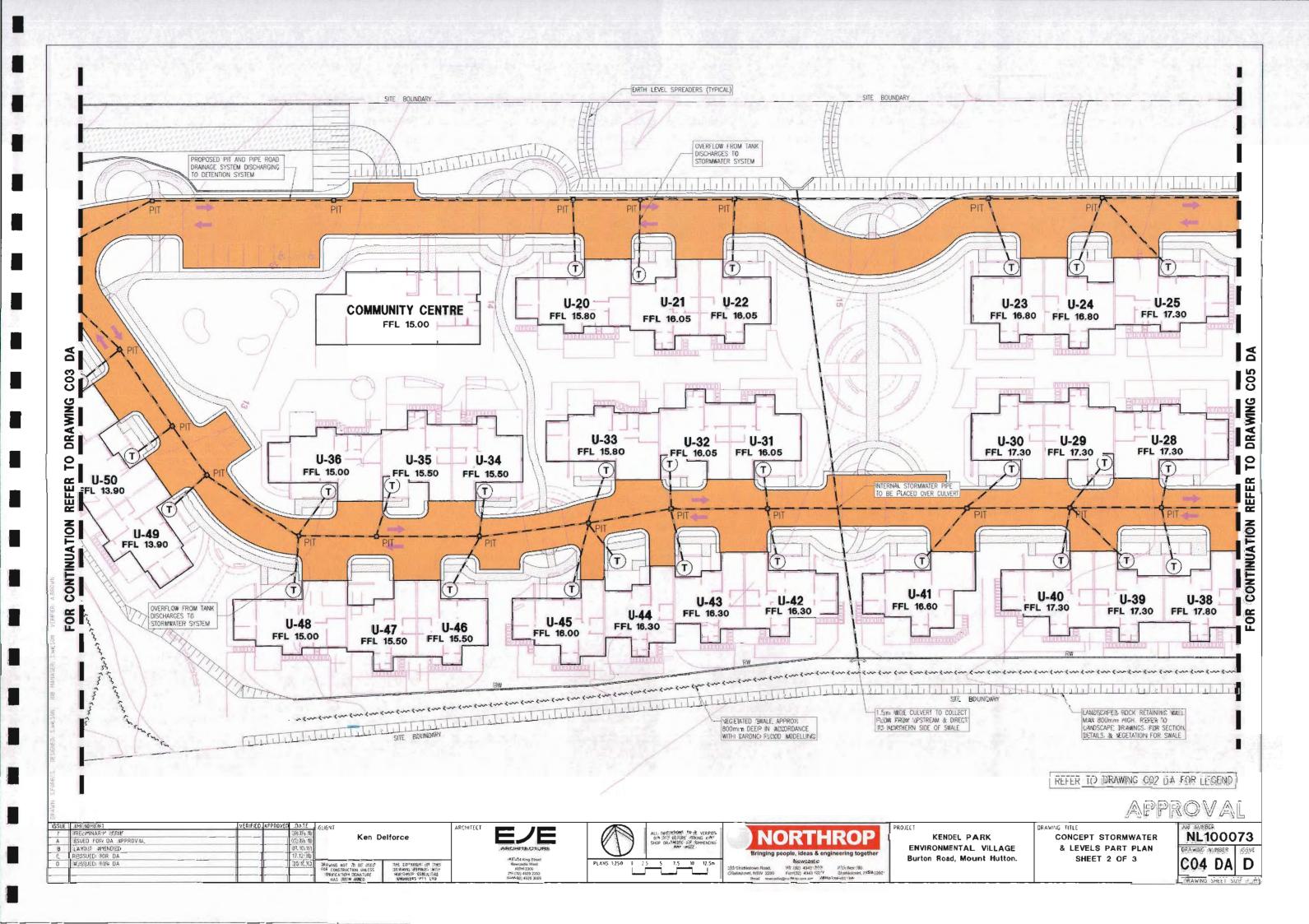
> INSTALL PIT PROTECTION TO ALL NEW & EXISTING STORMWATER PITS

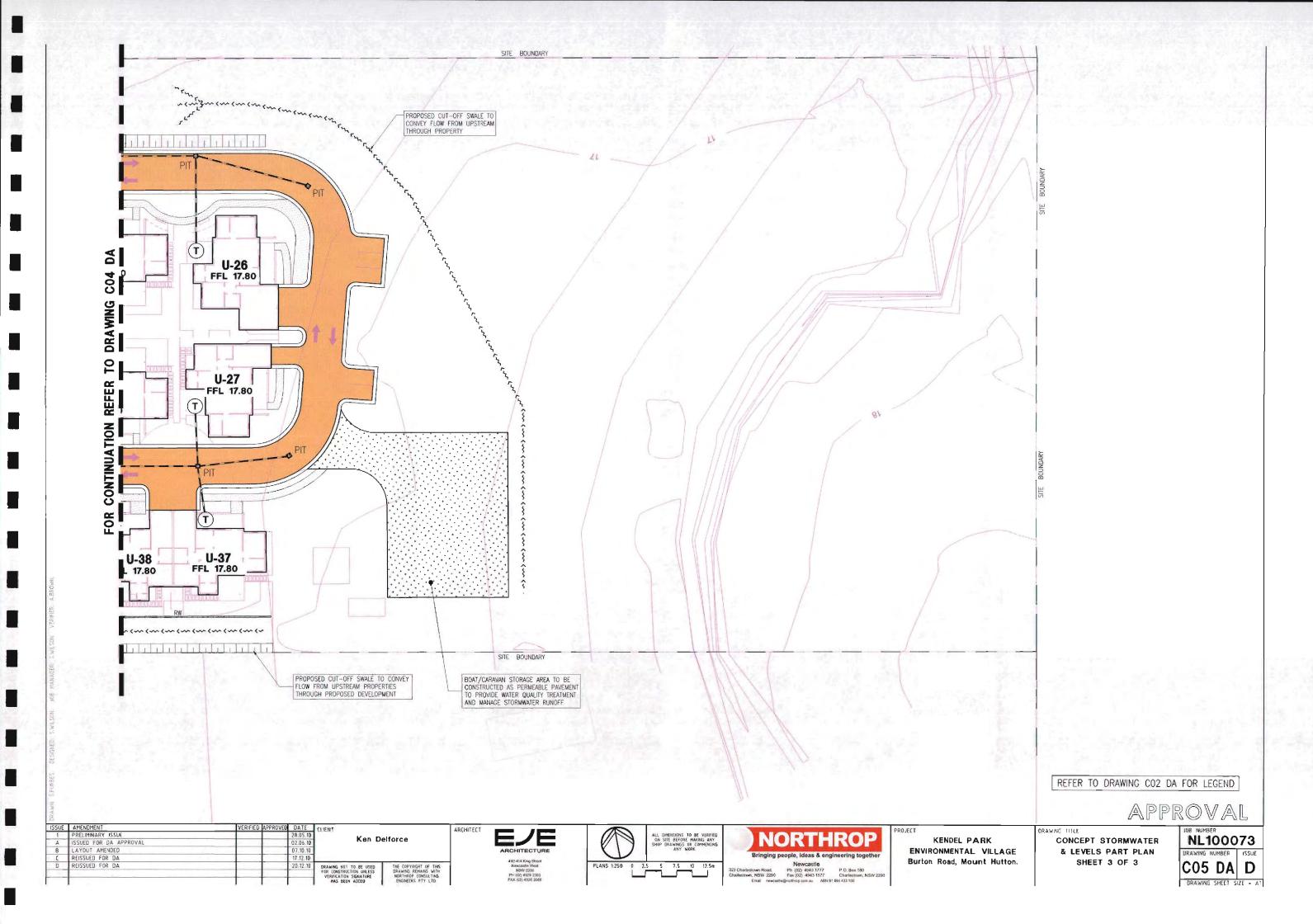
> > APPROVAL

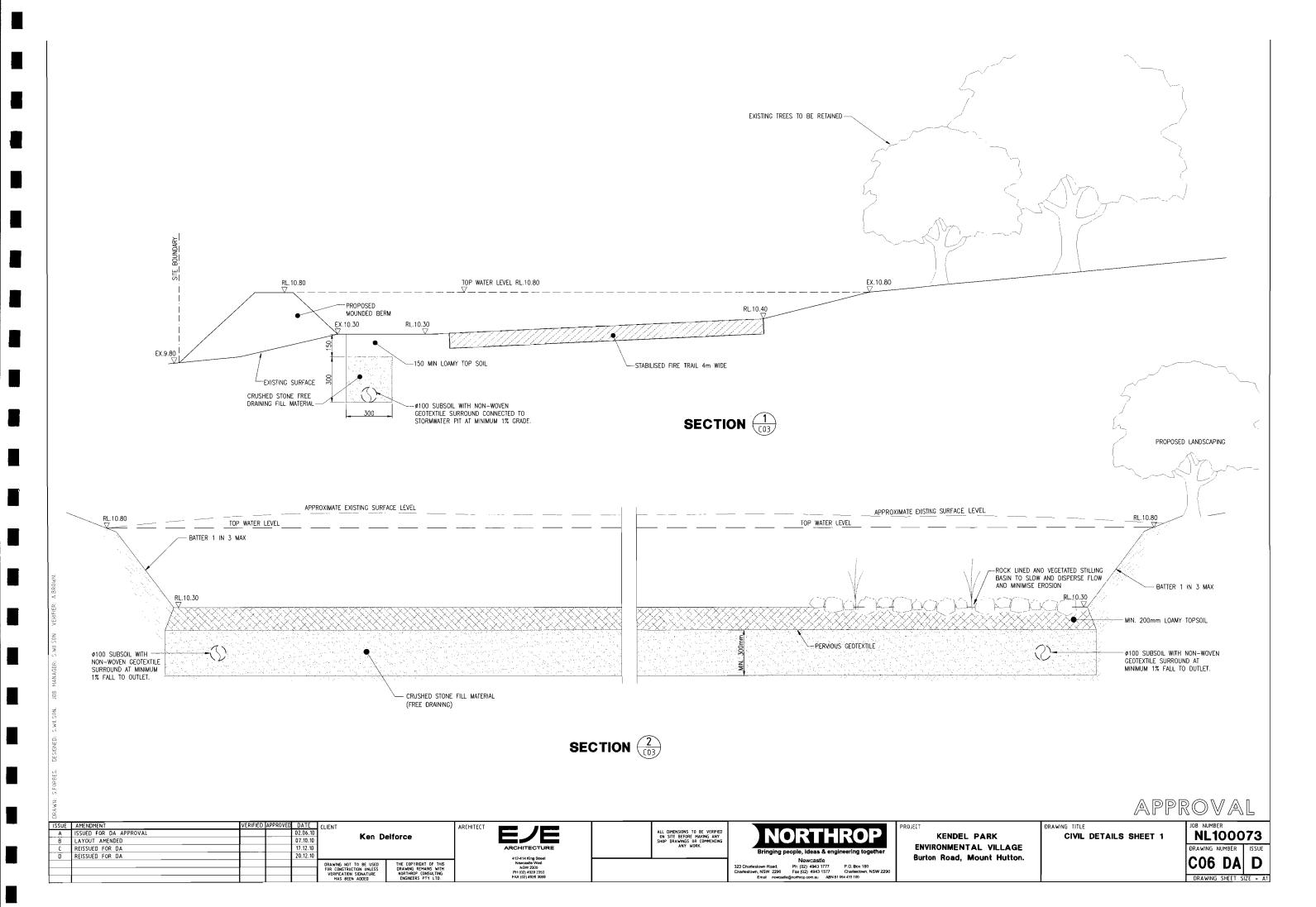
PRELIMINARY ISSUE NL100073 KENDEL PARK SEDIMENT & EROSION SUED FOR DA APPROVA ENVIRONMENTAL VILLAGE LAYOUT AMENDED CONTROL PLAN Burton Road, Mount Hutton. CO1 DA D EISSUED FOR DA PUANS 11750

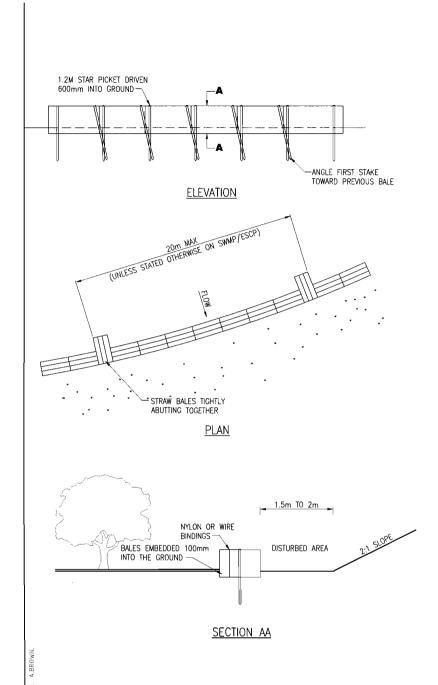












STRAW BALE FILTER SD 6-7

NOTES

1. CONSTRUCT THE STRAW BALE FILTER AS CLOSE AS POSSIBLE TO BEING PARALLEL TO THE CONTOURS OF THE SITE.

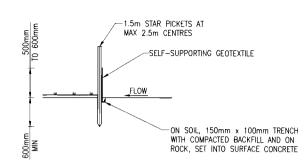
2. PLACE BALES LENGTHMISE IN A ROW WITH ENDS TIGHTLY ABUTTING. USE STRAW TO FILL ANY GAPS BETWEEN BALES. STRAWS ARE TO BE PLACED PARALLEL TO THE GROUND.

3. ENSURE THAT THE MAXIMUM HEIGHT OF THE FILTER IS ONE BALE.

4. EMBED EACH BALE IN THE GROUND 75mm TO 100mm AND ANCHOR WITH TWO 1.2m STAR PICKETS OR STAKES. ANGLE THE FIRST STAR PICKET OR STAKE IN EACH BALE TOWARDS THE PREVIOUSLY LAID BALE. DRIVE THEM 600mm INTO THE GROUND AND, IF POSSIBLE, FLUSH WITH THE TOP OF THE BALES. WHERE STAR PICKETS ARE USED AND THEY PROTRUDE ABOVE THE BALES, ENSURE THEY ARE FITTED WITH SAFETY CAPS.

5. WHERE A STRAW BALE FILTER IS CONSTRUCTED DOWN SLOPE FROM A DISTURBED BATTER, ENSURE THE BALES ARE PLACED 1 TO 2m DOWNSLOPE FROM THE TOE.

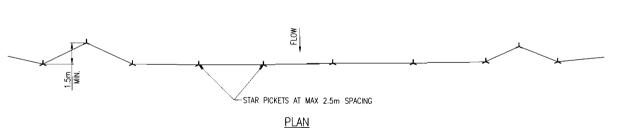
6. ESTABLISH A MAINTENANCE PROGRAM THAT ENSURES THE INTEGRITY OF THE BALES IS RETAINED — THEY COULD REQUIRE REPLACEMENT EACH TWO TO FOUR MONTHS.



SECTION DETAIL DISTURBED AREA -STAR PICKETS AT MAX 2.5m CENTRES UNDISTURBED AREA

ISOMETRIC VIEW

20m MAX (UNLESS STATED OTHERWISE BY SWMP/ESCP)



SEDIMENT FENCE SD 6-8

NOTES
1. CONSTRUCT SEDIMENT FENCES AS CLOSE AS POSSIBLE TO BEING PARALLEL TO THE CONTOURS OF THE SITE, BUT WITH SMALL RETURNS AS SHOWN IN THE DRAWING TO LIMIT THE CATCHMENT AREA OF ANY ONE SECTION. THE CATCHMENT AREA SHOULD BE SMALL ENOUGH TO LIMIT WATER FLOW IF CONCENTRATED AT ONE AREA SHOULD BE SMALL ENOUGH TO LIMIT WATER FLOW IF CONCENTRATED AT ONE POINT TO 50L/SEC IN THE DESIGN STORM EVENT, USUALLY THE 10-YEAR EVENT.

2. CUT A 150mm DEEP TRENCH ALONG THE UPSLOPE LINE OF THE FENCE FOR THE BOTTOM OF THE FABRIC TO BE ENTRENCHED.

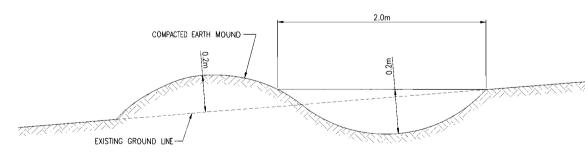
3. DRIVE 1.5m LONG STAR PICKETS INTO THE GROUND AT 2.5m INTERVALS (MAX) AT THE DOWNSLOPE EDGE OF THE TRENCH. ENSURE ANY STAR PICKETS ARE FITTED WITH SAFETY CAPS.

4. FIX SELF—SUPPORTING GEOTEXTILE TO THE UPSLOPE SIDE OF THE POSTS ENSURING IT GOES TO THE BASE OF THE TRENCH. FIX THE GEOTEXTILE WITH THE WIRE TIES OR AS RECOMMENDED BY THE MANUFACTURER. ONLY USE GEOTEXTILE SPECIFICALLY PROPOLICED FOR SENDIENT EFRICING. THE LISE OF SHADE CLOTH FOR

WINE IES ON AS RECOMMENDED BY THE MANUFACTURER. ONLY USE GEOTEXTILE SPECIFICALLY PRODUCED FOR SEDIMENT FENCING. THE USE OF SHADE CLOTH FOR THIS PURPOSE IS NOT SATISFACTORY.

5. JOIN SECTIONS OF FABRIC AT A SUPPORT POST WITH 150mm OVERLAP.

6. BACKFILL THE TRENCH OVER THE BASE OF THE FABRIC AND COMPACT IT THOROUGHLY OVER THE GEOTEXTILE.



TYPICAL CUT OFF **SWALE DETAIL**

| ISSUE | AMENOMENT | VERIFIED | APPROVED | DATE | CLIENT | | ARC |
|-------|-----------------|----------|----------|----------|---|---|-----|
| A | DETAILS ADDED | | | 07.10.10 | Ken Delforce | | - |
| В | REISSUED FOR DA | | | 17.12.10 | Ken D | enorce | |
| С | REISSUED FOR DA | | | 20.12.10 | | | |
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| | | | | | DRAWING NOT TO BE USED | THE COPYRIGHT OF THIS | 1 |
| | | | | | FOR CONSTRUCTION UNLESS VERIFICATION SIGNATURE | DRAWING REMAINS WITH NORTHROP CONSULTING | |
| | | | | | HAS BEEN ADDED ENGINEERS PTY | | l |

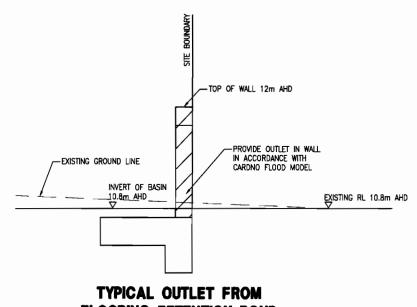




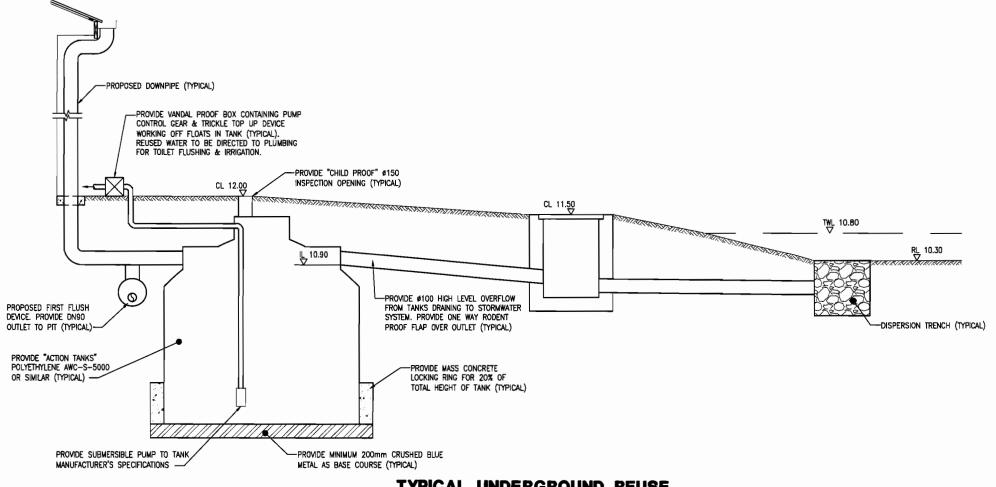
KENDEL PARK ENVIRONMENTAL VILLAGE Burton Road, Mount Hutton. RAWING TITLE CIVIL DETAILS SHEET 2

NL100073 DRAWING NUMBER CO7 DA C

DRAWING SHEET SIZE = A1



FLOODING RETENTION POND



TYPICAL UNDERGROUND REUSE TANK DETAIL (CRITICAL LOCATION)

| ISSU | AMENDMENT | VERIFIED | APPROVED | DATE | CLIENT | | ARCHITECT |
|------|-----------------|----------|-----------------|----------|---|---|-----------|
| A | REISSUED FOR DA | | | 17.12.10 | | elforce | , |
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| | | | | | FOR CONSTRUCTION UNLESS VERIFICATION SIGNATURE | GRAMING REMAINS WITH NORTHROP CONSULTING | l |
| | | | | | HAS BEEN ADDED | ENGINEERS PTY LTD. | 1 |
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| E/E ARCHITECTURE | ALL DIMENSIONS TO E ON SITE BEFORE MA SHOP DRAWINGS OR I ANY WORK |
|---|--|
| 412-414 King Street New castie Eviest NSW 2300 PH (02) 4929 2353 FAX (02) 4926 3069 | |



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NL100073 DRAWING NUMBER ISSUE CO8 DA B DRAWING SHEET SIZE = A1

LEGEND

DE

DENOTES 100 YEAR FLOOD EXTENT WITH 0.05m DEPTH

.....

DENOTES PMF FLOOD LEVEL

FFL 18.0

DENOTES PROPOSED FINISHED FLOOR LEVEL, FINISHED FLOOR LEVEL SET A MINIMUM 500mm ABOVE 1% AEP FLOOD EVENT

APPROVAL

A REISSUED FOR DA 17.12.10

B REISSUED FOR DA 20.17.10

B REISSUED FOR DA 20.17.10

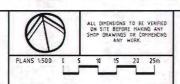
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Burton Road, Mount Hutton.

PRAWING TITLE
FLOODING EXTENTS PLAN

DRAWING SHEET SIZE = A1



Appendix C - Table Drain Calculations, Burton Road

Peak flows from basin, modelled in XP-RAFTS:

10 year ARI = $0.8 \text{m}^3/\text{sec}$ 100 year ARI = $1.6 \text{m}^3/\text{sec}$

The surveyed table drain (survey data provided by de Witt Consulting) was modelled in HEC-RAS to assess flow capacity.

HEC-RAS Modelling Results:

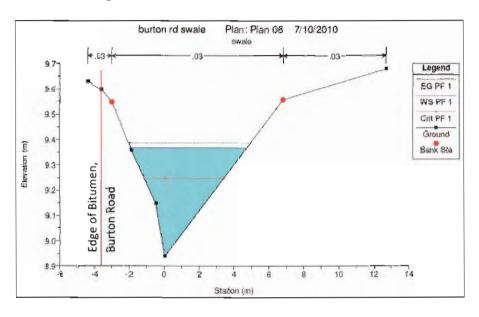


Figure D1 - 10 year ARI peak flow from basin within existing swale adjacent to Burton Rd

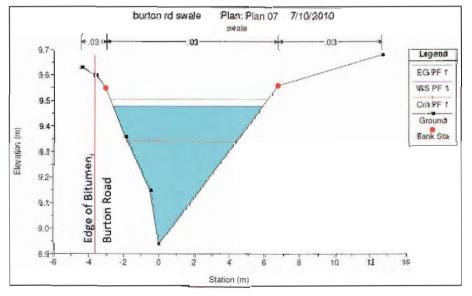


Figure D2 - 100 year ARI peak flow from basin within existing swale adjacent to Burton Rd